sij' ravne steel

HOT WORK TOOL STEEL

RAVNEX

RS 450

Family of RS hot-work tool steel

HOT WORK TOOL STEEL

GRADE RS		W. Nr.	DIN	AISI
RS 400		1.2343	X38CrMoV5-1	H11
RS 410		1.2344	X40CrMoV5-1	H13
RS 420		1.2367	X38CrMoV5-3	-
RS 431		1.2345	X50CrMoV5-1	
RS 432		1.2362	X63CrMoV5-1	
RS 433		1.2365	X32CrMoV33	H10
RS 435		1.2714	56NiCrMoV7	
RS 440	RAVNEX	1.2343 Mod.	X38CrMoV5-1 Mod.	H11 Mod.
RS 450	RAVNEX			

CONTENTS

GENERAL CHARACTERISTICS				4
Chemical composition				
Application				
Microstructure in delivered condition				
Toughness				
Qualitative comparison				
PHYSICAL PROPERTIES				7
MECHANICAL PROPERTIES				8
Impact toughness at elevated temperatures				
CONTINIOUS COOLING CURVES-CCT				9
HEAT TREATMENT				10
Stress relieving				
Hardening				
Tempering				
Dimensional changes during hardening and tempe	ring	5		
SURFACE TREATMENT				12
WELDING AND EDM				13
Electrical discharge machining				
RECOMMENDATIONS FOR MACHINING				14
CASE STUDY				15

GENERAL CHARACTERISTICS

RS 450 RAVNEX is a supreme hot-work tool steel produced in METAL RAVNE, known for:

- Excellent impact toughness
- High hot tensile properties and high working hardness
- Excellent thermal conductivity
- Good polishability
- Excellent hardenability
- Nitrability

- High cleanliness
- Longer tool life
- · Excellent homogeneity
- Weldability



RS CHEMICAL COMPOSITION (%)

Controlled chemical composition with minimal content of detrimental elements compared to standard steel grades. Cleanliness according to DIN 50602 is K1≤10.

RS GRADE	AISI	W. Nr.	С	Si	Mn	Cr	Мо	V	Ni
RS 450 RAVNEX	-	-	0,37	0,25	0,43	4,90	1,60	0,59	1,60

Chemical element content is in wt.%

ightarrow RS APPLICATION

RS 450 RAVNEX is primarily designed for die casting of light metals and alloys. Due to its excellent hardenability it is especially recommended for high-dimension tooling. It is often used for highly stressed hot-work structural parts where superior toughness is required.

RS 450 RAVNEX is also recommended for die forging and extrusion. Because of its good polishability, the grade can be used for plastic molding applications and processing of glass.

RS 450 RAVNEX is supplied in annealed condition, max. 235 HBW (791 N/mm²).

GENERAL CHARACTERISTICS

ightarrow MICROSTRUCTURE IN DELIVERED CONDITION

RS 450 RAVNEX is inspected in soft annealed condition according to SEP 1614 (Stahl-Eisen-Prüfblatt SEP 1614 - September 1996), and according to NADCA#207 standard.

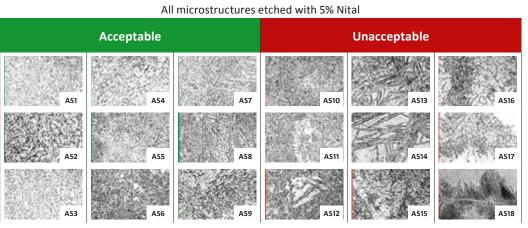
→ TAB 1: MICROHOMOGENEITY

Increasing Reduction Ratio

Premium quality		Standard quality		Not acceptable
SA	SB	SC	SD	SE
SA1	SB1	SC1	SD1	SE1
SA2	SB2	sc2	SD2	SE2
SA3	SB3	SC3	SD3	SE3
SA4	SB4	SC4	SD4	SE4
	Increasing Degree	e of Segregation		▶ 50 ×

Accepted rating charts of annealed RS 450 RAVNEX.

→TAB 2: ACCEPTABILITY CRITERIA OF ANNEALED MICROSTRUCTURE ACCORDING TO NADCA #207-2003



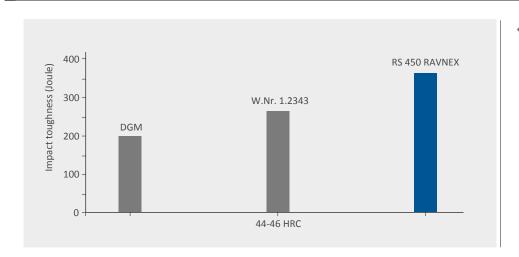
500 ×

GENERAL CHARACTERISTICS

TOUGHNESS

Un-notched specimens (7 \times 10 \times 55 mm) are used to test impact toughness in transverse direction, SEP 1314 (Stahl-Eisen-Prüfblatt SEP 1314- April 1990). Specimens are quenched and tempered to 45 +/- 2 HRC, and test is performed at 20 $^{\circ}$ C.

Average impact toughness of forged quality is higher than 299 Joule for average forging size of 900×400 mm.



DGM (Deutsche Gesellschaft für Materialkunde) recommends impact toughness of minimum 200 Joules for hot-work tool steel in various hotwork applications.

ightarrow QUALITATIVE COMPARISON

RS 450 RAVNEX is a premium tool steel of highest toughness produced in Metal Ravne. Chart shows its toughness at high temperature compared to RS400, conventional W.Nr1.2344 hot-work tool steel and to RS 440 RAVNEX. Tool steel with increased toughness at high temperature is critical in applications where there is risk of gross cracking. Properties are measured at $600\,^{\circ}$ C.



STRENGTH means
 ultimate tensile
 strength derived from
 an engineering stress strain curve.
 TOUGHNESS is
 estimated by reduction
 in cross-section area
 of tensile test probe at
 rupture.

PHYSICAL PROPERTIES

NOTES

DENSITY (g/cm³)				
7.83 (20 °C)	7.70 (450 °C)	7.68 (500 °C)	7.66 (550 °C)	7.65 (600 °C)
				•
THERMAL CONDU	CTIVITY (W/(m.K))			
32.80 (100 °C)	34.30 (450 °C)	34.10 (500 °C)	33.90 (550 °C)	33.50 (600 °C)
	'		1	ı
FIFCTRIC RESISTIN	VITY (Ohm. mm²/m)			
0.50 (100 °C)	0.58 (450 °C)	0.63 (500 °C)	0.68 (550 °C)	0.73 (600 °C)
. ,		, ,	, ,	
SPECIFIC HEAT CA			I	I
0.44 (20 °C)	0.64 (450 °C)	0.68 (500 °C)	0.72 (550 °C)	0.83 (600 °C)
MODULUS OF ELA	STICITY (10°xN/mm°)			
MODULUS OF ELA 210 (20 °C)	STICITY (10³xN/mm²)			
	STICITY (10 ³ xN/mm ²)			
210 (20 °C)	STICITY (10³xN/mm²)	ION (10 ⁻⁶ °C ⁻¹ , 20 °C)*		

 * CTE is the mean coefficient of thermal expansion with reference temperature of 20 °C.

M E C H A N I C A L P R O P E R T I E S

> IMPACT TOUGHNESS AT ELEVATED TEMPERATURES

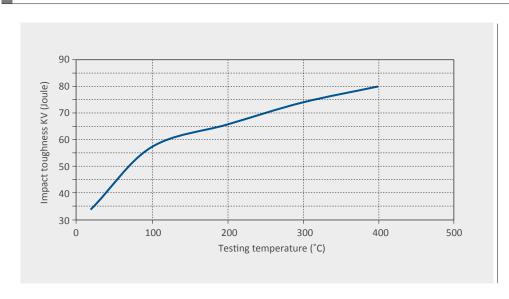


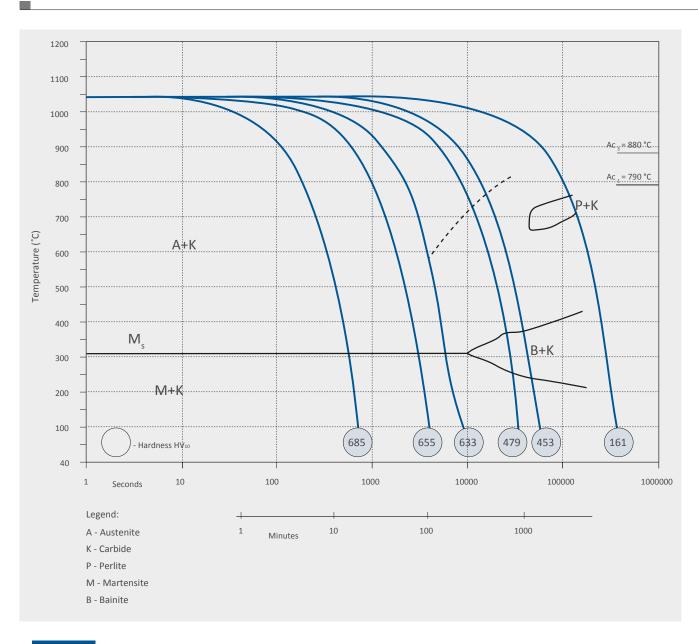
Figure shows impact toughness as function of temperature. Samples are taken from the core of a forged block in short transverse direction.

They are quenched and tempered
(Q+T; 1030 °C / oil / 2x tempering) to 45 +/- 1

HRC. Measurement:
EN ISO 148: 2010

CONTINIOUS COOLING CURVES-CCT

Austenitising temperature: 1030 °C; soak time: 15 min



TIP 1

Quench rate should be sufficient to form predominantly martensitic structure without

significant amount of bainite. Significant amount of bainite favours thermal fatigue as a less stable phase constituent with lower strength.



NOTES

Recommendations or NADCA#207.

ightarrow ANNEALING

HEATING	ANNEALING TEMPERATURE	COOLING
50 °C/h	800 - 850 °C	20 °C/h
Protect against oxidation, scaling and decarburisation.	Min. 4 hours.	Slow in furnace. From 600 °C air cooling is possible.

ightarrow STRESS RELIEVING

HEATING	STRESS RELIEVING	COOLING
100°C/h	650 °C or 50 °C under the last tempering temperature.	20°C/h
Protect against oxidation and decarburisation.	Min. 3 hours.	Slow and uniformly in the furnace to prevent formation of additional residual stresses. From approximately 200 °C air cooling is possible.

→ HARDENING

Hardness after hardening is 56-58 HRC (2030 - 2180 N/mm²).

HEATING	AUSTENITISING	COOLING
25 - 650 °C, 150-220 °C/h 650 - 850 °C, ≤150 °C/h 850 - 1030 °C, ≤150 °C/h	1030 - 1050 °C	See CCT diagram
Hold in furnace at $T = 650 ^{\circ}\text{C} / 850 ^{\circ}\text{C}$ until $T_{\text{SURFACE}} - T_{\text{CORE}} \le 110 ^{\circ}\text{C} / 60 ^{\circ}\text{C}$	T _{SURFACE} is measured at 15mm underneath surface, maximum soak time is 30 min.	Fast cooling is recommended in pressurized $\rm N_2$. For large dimension hot-work tooling see NADCA#207 or GM DC-9999-1Rev.18 specification.



For applications exposed to extreme thermal loading a proper heat treatment is essential.

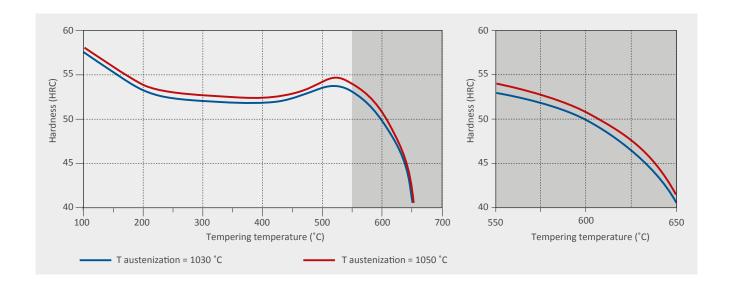
To prevent excessive grain growth during austenitization it is preferable to leave some of the carbides not dissolved.

H E A T T R E A T M E N T

ightarrow TEMPERING

Tempering must start immediately after completion of quenching (when part reaches 90-70 $^{\circ}$ C). Three tempering treatments are recommended. First tempering destabilizes retained austenite. Second tempering tempers newly formed microstructure constituents.

HEATING	TEMPERING TEMPERTAURE	COOLING
150 °C/h – 250 °C/h	1st: 540 - 550 °C 2nd: choose working hardness (see tempering diagram). 3rd: 50 °C bellow 2nd tempering.	Cool in air or in the furnace to room temperature between tempering cycles.
Protect against oxidation and decarburisation.	1 hour per 25mm wall thickness based on the furnace temperature. Minimum 2 hours.	



TIP 3

Increased toughness of this special grade offers one to select higher working hardness.

→ Higher thermal conductivity and high temperature strength compared to H11 grade also contribute to its improved resistance to thermal fatigue.

ightarrow DIMENSIONAL CHANGES DURING HARDENING AND TEMPERING

It is recommended to leave machining allowance before hardening of minimum $0.2\,\%$ of dimension, equal in all three directions.

SURFACE TREATMENT

ightarrow NITRIDING AND NITROCARBURISING

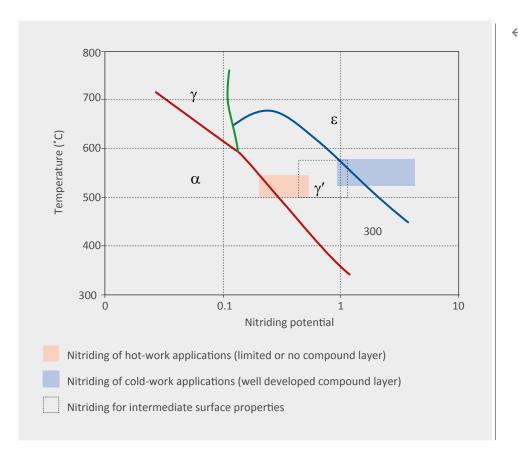
Nitriding treatment is commonly recommended to enhance surface properties of **RS 450 RAVNEX.**

Nitriding treatment for hot-work applications is performed by producing diffusion zone only (α nitriding phase) of a depth determined by particular application requirements, and completely inhibit surface compound layer (γ' and ϵ nitriding phases).

Nitriding treatment for plastic-molding or cold-work applications with wear resistance requirements is performed by producing surface compound layer of composition and thickness determined by particular application requirements.

For applications with requirement for additional surface protection, improvement of sliding properties, or improvement of corrosion resistance, it is recommended that oxidation treatment (Fe_3O_4) follows the nitriding.

For details on surface preparation and setup of nitriding treatment parameters to obtain required surface properties please consult our approved nitriding specialist.



Lehrer diagram presented in figure shows the effect of two parameters: (1) nitriding potential (a function of partial pressure of ammonia and hydrogen), and (2) temperature, on composition of nitriding phases formed on material surface. Figure shows recommended selection of the two governing parameters for appropriate execution of nitriding for two extreme application regimes, hot work on one hand, and cold-work on the other.

WELDI	
ANDE	OM

NOTES

ightarrow WELDING

RS 450 RAVNEX is a readily weldable alloy by TIG or MMA welding processes in hardened or soft-annealed condition. Filler metal should be of the same or similar chemical composition.

Heat treatment after welding is recommended. Annealing should be performed after welding of soft annealed parts, whereas tempering at temperature of about 50°C below tempering temperature should be performed after welding of hardened and tempered parts. Laser welding is recommended for repair of smaller cracks and edges.

PREHEATING TEMPERATURE	MAXIMUM INTERPASS TEMPERATURE	POST WELD COOLING
320 °C	470 °C	Approximately 30 °C / h to not less than 70 °C, then tempering.

WELDING METHOD FILLER MATERIAL		HARDNESS AFTER WELDING
TIG, MMA	H11, exceptional H13	~ 50 HRC

ELECTRICAL DISCHARGE MACHINING

Electrical discharge machining (EDM) leaves a brittle surface layer due to melting and resolidification of surface material.

It is recommended to: (1) remove the resolidified layer by polishing, grinding or other mechanical methods, and (2) temper the work-piece at temperature of about 50 °C below the tempering temperature. Execution of tempering of re-hardened and jet untempered layer underneath the surface is critical.

RECOMENDATIONS FOR MACHINING

 NOTES

The information below is provided solely as a general machining guideline. It refers to material in soft annealed condition.

DRILLING

INSERT	DRILL DIAMETER (mm)	CUT TING SPEED (m/min)	FEED (mm/rev)
K15 - K20	5 - 20	70	0.05 - 0.15

FACE MILLING

INSERT	CUTTING SPEED (m/min)	FEED (mm/tooth)	DEPTH OF CUT (mm)
P30-P40 c.* (rough milling)	60 - 100	0.20	- 2.00
P10-P20 c.* (fine milling)	75 - 130	0.20	- 2.00

ightarrow TURNING

INSERT	CUTTING SPEED (m/min)	FEED (mm/rev)	DEPTH OF CUT (mm)
P30-P40 c.* (rough turning)	65 - 100	- 1.00	- 4.00
P10 c.* (fine turning)	140 - 200	- 0.30	- 2.00

^{*} c. = coated carbide



ightarrow HEAT TREATMENT OF RS 450 RAVNEX

Control of quenching is critical to assure dimension stability, optimum microstructure and mechanical properties of any work-piece. Finite element modelling of heat treatment reveals that both hardening temperature and soaking time, as well as quenching rate strongly depend on work piece size and geometry.

→ FIG 1

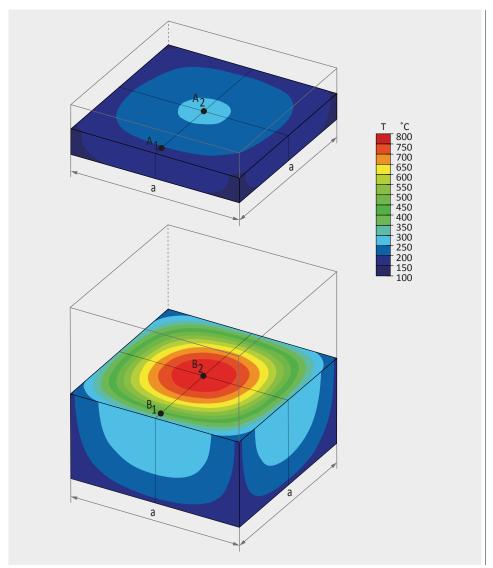


Figure 1 shows temperature distribution in two workpieces of different thickness at a given time (t), (see Figure 2) during quenching. One can observe a hot core and a high temperature gradient in a thick workpiece, while a thin workpiece has at same cooling time almost uniform temperature distribution.

CASE STUDY

→ FIG 2

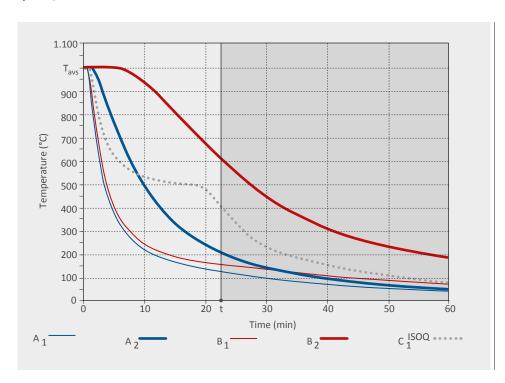


 Figure 2 reveals temperature transient at quenching for both workpieces at two characteristic points: (1) a point 15mm underneath the surface, and (2) the core.

→ FIG 3

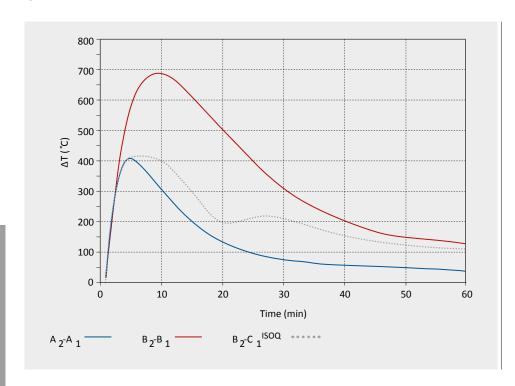


Figure 3 shows temperature difference between the two characteristic points for both workpieces for the same quenching transient. An extreme temperature gradient occurs in the thick workpiece, with high risk of causing distortion or gross cracking. Application of isothermal quenching process (see NADCA#207) is recommended to reduce the potential detrimental effects of extreme temperature difference. A short isothermal hold reduces significantly the temperature gradient in the thick workpiece. (See surface temperature transifnt curve C1ISOQ in Figure 2 and Figure 3.)

CASE STUDY

To achieve optimum material properties, heat treatment parameters should be adjusted to specific workpiece size and geometry. Critical quench rate is needed to avoid both pearlite formation and carbide precipitation.

In order to run quenching of a particular dimension and geometry workpiece at optimum velocity it is critical to continuously monitor temperature of both the surface and the core throughout the cycle.

→ FIG 4

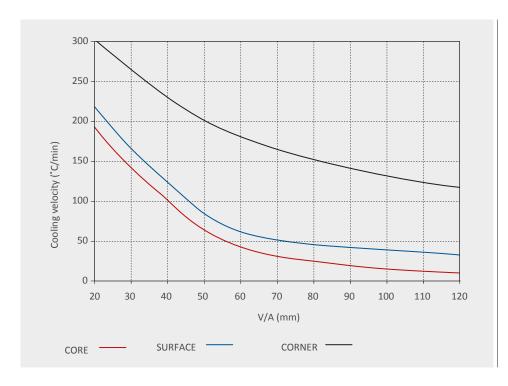


Figure 4 shows average cooling speed between 800 and 500°C at the core of a generalized geometry workpiece. Both geometry and size of the workpiece is defined by its volume (V) to surface (S) ratio. Medium quenching power in a vacuumtype furnace is applied to determine the workpiece cooling speed (6bar N2 overpressure with medium to high gas circulation). The plot is particularly useful for determining optimum quenching speed in workpieces where temperature at core is not possible to directly monitor by thermocouple.

SURFACE – temperature at a point 15 mm underneath the center of largest workpiece surface.

CORNER* – temperature at a point 15 mm underneath the most exposed part of workpiece.

* data presented are computed for a point 15mm underneath an angle of a cube.



Sharp edges on the tool in heat treatment should be avoided to prevent gross cracking or micro quenching cracks which can lead to formation of leading cracks.

×
ш
5
>
4
0
0
20
15(
2
15(
45(
RS 45 (
3 45(



RS 450 RAVNEX is produced by:

Metal Ravne d.o.o. Koroška cesta 14 2390 Ravne na Koroškem Slovenia

www.metalravne.com

RS 450 RAVNEX is distributed by:

Ravne Steel Center d.o.o.

Litostrojska cesta 60 1000 Ljubljana Slovenia

info@rsc.si

